

PROB # 4-12

LRFD	ASD
$P_u = (1.2)(450) + (1.6)(120) = 732 \text{ k}$	$P_u = 450 + 120 = 570 \text{ k}$

(a)  $\text{Min. } A_g = \frac{P_u}{\phi_t F_y} = \frac{732}{(0.90)(36)} = 22.59 \text{ in.}^2 \leftarrow$

(b) Assume  $u = 0.90$  after study of AISC Table I-1 & Table D3-1

$\text{Min } A_g = \frac{P_u}{\phi_t F_u u} + \text{Estimated } A \text{ of holes}$

$= \frac{732}{(0.75)(58)(0.90)} + (4)\left(\frac{3}{4} + \frac{1}{8}\right)(0.735) = 21.27 \text{ in.}^2$

(c)  $\text{Min preferable } r = \frac{(12)(24)}{390} = 0.96 \text{ in.}$

Try W12x79 ( $A = 23.2 \text{ in.}^2$ ,  $d = 12.4 \text{ in.}$ ,  $r_x = 0.735 \text{ in.}$ ,  $r_y = 3.05 \text{ in.}$ )

$\bar{x} = \bar{y} = 1.06 \text{ in. for a WT } 6 \times 39.5 \text{ (} b_f = 12.1 \text{ in.)}$

Checking

(a)  $P_m = F_y A_g = (36)(23.2) = 835.2 \text{ k}$

LRFD $\phi_t = 0.90$	ASD $\Omega_t = 1.67$
$\phi_t P_m = (0.90)(835.2) = 751.7 \text{ k} > 732 \text{ k}$	$\frac{P_m}{\Omega_t} = \frac{835.2}{1.67} = 500.1 < 570 \text{ k} \text{ N.G.}$

(b)  $u = 1 - \frac{\bar{x}}{L} = 1 - \frac{1.06}{4} = 0.735$

But AISC Table D3.1 Case 7 says  $u = 0.90$  if  $b_f > \frac{2}{3}d$

$b_f = 12.1 > \frac{2}{3} \times 12.4 = 8.27 \text{ in. } \therefore u = 0.90$

$A_m = 23.2 - (4)\left(\frac{3}{4} + \frac{1}{8}\right)(0.735) = 20.63 \text{ in.}^2$

$A_e = u A_m = (0.90)(20.63) = 18.57 \text{ in.}^2$

$P_m = F_u A_e = (58)(18.57) = 1077.1 \text{ k}$

LRFD $\phi_t = 0.75$	ASD $\Omega_t = 2.00$
$\phi_t P_m = (0.75)(1077.1) = 807.8 \text{ k} > 732 \text{ k}$	$\frac{P_m}{\Omega_t} = \frac{1077.1}{2.00} = 538.5 \text{ k} < 570 \text{ k} \text{ N.G.}$

Ans.

W12x79

W12x87

*v g c m c*

PROB # 4-20

LRFD	ASD
<p>Truss loads</p> $P_u = (1.2)(30) + (1.6)(24) = 74.4 \text{ k}$ <p>By analysis of the truss force in member L2L3 is equal to 446.4 k</p>	<p>Truss loads</p> $P_a = 30 + 24 = 54 \text{ k}$ <p>By analysis of the truss the force in member L2L3 = 324 k</p>

(a)  $\text{Min. } A_g = \frac{446.4}{(0.9)(36)} = 13.79 \text{ in.}^2$

(b)  $\text{Min. } A_g = \frac{P_u}{\phi_t F_u \mu} + \text{Estimated area of holes}$

Assume  $\mu =$  about 0.8 after studying AISC Table D3.1

$\text{Min. } A_g = \frac{446.4}{(0.75)(58)(0.8)} + (-)\left(\frac{3}{4} + \frac{1}{8}\right)(\text{estimated } \frac{3}{4} \text{ in.}) = 14.14 \text{ in.}^2$

(c)  $\text{min. preferable } r = \frac{L}{300} = \frac{(12)(12)}{300} = 0.48 \text{ in.}$

After studying double angle tables (AISC 1-15)

Try 2L5 8x4 x  $\frac{5}{8}$  ( $A = 14.3 \text{ in.}^2$ ,  $\bar{x} = 0.902$ ,  $r_y = 1.52$ )

Checking

(a)  $P_m = F_y A_g = (36)(14.3) = 514.8 \text{ k}$

LRFD $\phi_t = 0.90$	ASD $\Omega_t = 1.67$
$\phi_t = (0.90)(514.8) = 463.3 \text{ k} > 446.4 \text{ k}$	$\frac{P_m}{\Omega_t} = \frac{514.8}{1.67} = 308.3 \text{ k} < 324 \text{ k}$ <u>NG</u>

PROB # 4-20 CONTD

$$(b) u = 1 - \frac{r}{L} = 1 - \frac{0.992}{2 \times 4} = 0.89$$

$$A_m = 14.3 - (4) \left( \frac{3}{4} + \frac{1}{8} \right) \left( \frac{5}{8} \right) = 12.11 \text{ in.}^2$$

$$P_m = F_u u A_m = (58)(0.89)(12.11) = 625.1 \text{ k}$$

LRFD $\phi_t = 0.75$	ASD $\Omega_t = 2.00$
$\phi_t P_m = (0.75)(625.1) = 468.8 \text{ k} > 446.4 \text{ k}$	$\frac{P_m}{\Omega_t} = \frac{625.1}{2.00} = 312.5 \text{ k} < 324 \text{ k}$
	<u>N.G.</u>

$$(c) \frac{L}{r} = \frac{(12)(12)}{1.52} = 94.7 < 300 \text{ OK}$$

ANS.

USE 2Ls 8x4 x  $\frac{5}{8}$   
For LRFD

USE 2Ls 8x4 x  $\frac{3}{4}$   
For ASD

*vjc mc*

PROB # 4-24

LRFD	ASD
$P_u = (1.2)(10) + (1.6)(12) = 31.2 \text{ k}$	$P_a = 10 + 12 = 22 \text{ k}$

$$A_D \geq \frac{P_u}{\phi 0.75 F_u} = \frac{31.2}{(0.75)(0.75)(58)} = 0.956 \text{ in.}^2$$

Try  $1\frac{1}{8}$  in. diameter rod from AISC Table 7-18  
using the gross area of the rod  $0.994 \text{ in.}^2$

$$R_m = 0.75 F_u A_D = (0.75)(58)(0.994) = 43.24 \text{ k}$$

LRFD $\phi = 0.75$	ASD $\Omega = 2.00$
$\phi R_m = (0.75)(43.24) = 32.43 \text{ k}$ $> 31.2 \text{ k}$ <u>ok</u>	$\frac{R_m}{\Omega} = \frac{43.24}{2.00} = 21.62 \text{ k} \approx 22 \text{ k}$ <u>ok</u>

USE  $1\frac{1}{8}$  in. diameter rod with  
7 threads per inch for  
LRFD and ASD

✓ gcm