

Exam Thursday  
every  
other  
seat

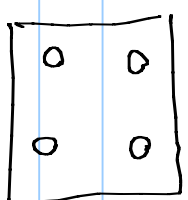
Steel Ch 3, 4, 5, 6 HW 2, 3, 5, 6  
tens. comp.

Concrete Ch 9 HW 4  
comp.

Equation Sheet  
Tables

# Concrete Columns

9,10



Design square tied column

$$P_D = 280k, \quad P_L = 500k, \quad f'_c = 4 \text{ ksi}, \quad f_y = 60 \text{ ksi}$$

$$\rho = 0.02 \quad (\text{2\% steel}) \quad 0.01 \leq \rho \leq 0.08$$

$$\phi P_n = \alpha_{\text{eccent.}} \phi \left[ \underbrace{(0.85 f'_c)}_{\text{spalling}} (A_g - A_{st}) + A_{st} f_y \right] \leq \phi P_u$$

$$\phi P_n \geq P_u$$

$$P_u = 1.2(280k) + 1.6(500k) = 1,136k$$

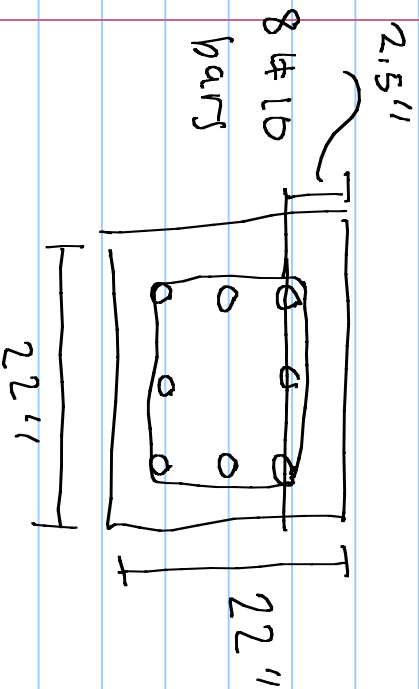
$$\alpha_{\text{tied}} = 0.80, \quad \phi_{\text{tied}} = 0.65$$

$$1,136 \text{ k} = (.80)(.65) \left[ (.85 \times 4)(A_g - .02A_g) + .02A_g(60) \right]$$

$$A_g = \underline{482} \text{ in}^2 \quad 22' \times 22'' \quad A_g = 484 \text{ in}^2$$

$$A_{st} = 0.02(482) = 9.64 \quad (\text{eg. } 9.52)$$

$$8 \# 10 \text{ bars} \quad A_{st} = 10.12 \text{ in}^2$$



Check

$$\phi P_n = (.8)(.65) \left[ (.85 \times 4)(484 - 10.12) + (10.12)60 \right]$$

$$= 1,154 \text{ k} > 1,136 \text{ k} \quad \checkmark$$

$$P = 10.12 / 484 = 0.021 \leq .08 \quad \checkmark$$

## Steel Column Review

Section 5.1 - 5.10

Section 6.1 - 6.2

### Column Design

- Hand Calculations
  - Guess  $F_c \approx 0.75 F_y$
  - Choose area
  - Check and iterate
- Design Charts
  - Find  $(K L)_y$  and  $P_u$
  - Choose Preliminary sections
  - Check strong axis buckling using  $K L_{eff} = \frac{(K L)_x}{r_x / r_y}$
  - Check and iterate

Example. 6-15

Find lightest W14 section

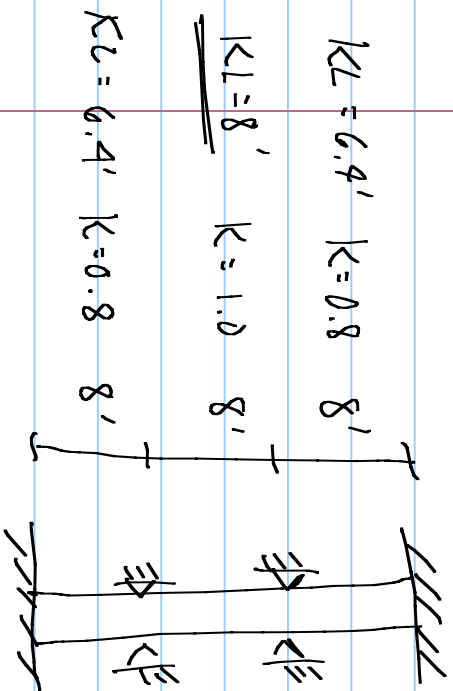
$$P_u = 912 \text{ k}$$

$$L = 24'$$

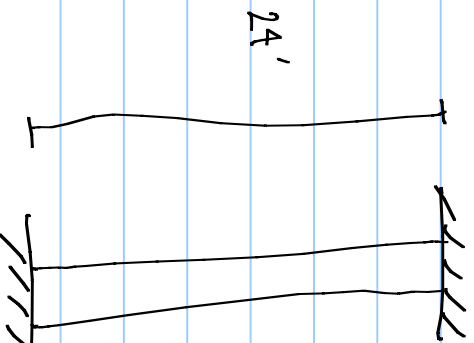
Grade 50

Fixed at top and bottom

Weak axis braced 8' from each end. (Pinned)



Weak Axis



Strong Axis

$$L_y = 8'$$
$$(K L)_y = 8'$$

Try W14 x 82.

$$r_x / r_y = 2.44$$

Strong Axis:  $K L_{eff} = \frac{0.65 (\cancel{10.8})(24')}{2.44} = 6.39' < 8' \therefore \underline{OK}$

Use W14 x 82

## Tension Members

Limit States: Yielding,  $\phi P_n = \phi F_y A_g$  ( $\phi = 0.9$ )  
Fracture,  $\phi P_n = \phi F_u A_e$  ( $\phi = 0.75$ )

$$A_e = U A_n$$

Slenderness Limit,  $L/r < 300$

$$r = r_{min}$$

Tension Rods,  $\phi P_n = \phi 0.75 F_u A_g$  ( $\phi = 0.75$ )  
Slenderness Limit  $N/A$

## Tension Member Example (4.11)

Choose lightest W10

$$P_u = 264 \text{ kips}$$

Grade 50

Member is connected w/ longitudinal welds,  $U = 0.87$   
 $L = 18'$

Design Based on Yielding

$$\phi P_n = 0.9 F_y A_g \geq P_u$$

$$A_g \geq \frac{P_u}{0.9 F_y} = \frac{264 \text{ k}}{0.9 (50 \text{ ksi})} = 5.87 \text{ in}^2$$

## Design Based on Fracture

$$\phi P_n = 0.75 F_u A_e \geq P_u$$

$$0.75 F_u (U A_n) \geq P_u \quad (A_n = A_g \text{ for welded})$$

$$0.75 F_u U A_g \geq P_u$$

$$A_g \geq \frac{P_u}{0.75 U F_u} = \frac{264 \text{ kips}}{0.75 (0.87) (65 \text{ ksi})} = 6.22 \text{ in}^2$$

$$\text{Choose } W10 \times 22 \quad (A_g = 6.49 \text{ in}^2)$$

$$\text{Check slenderness: } \frac{L}{r_{\min}} = \frac{(18 \text{ ft})(12 \text{ in/ft})}{1.33 \text{ in}} = 162 < 300 \quad \checkmark$$

Use  $W10 \times 22$ .