

Tension Member Design

- Select area based on yielding and fracture limit states

$$(1) A_g \geq \frac{P_u}{0.9F_y} \quad (\text{yielding})$$

$$(2) A_g \geq \frac{P_u}{0.75F_u U} + \frac{A_{bh}}{U}$$

May need to estimate for preliminary design

- Slenderness Requirement: $L/r_{\min} \leq 300$

r = radius of gyration

Example 1. (4-1).

Select the lightest W14 section available to support tensile loads of $P_D = 220$ k and $P_L = 250$ k.

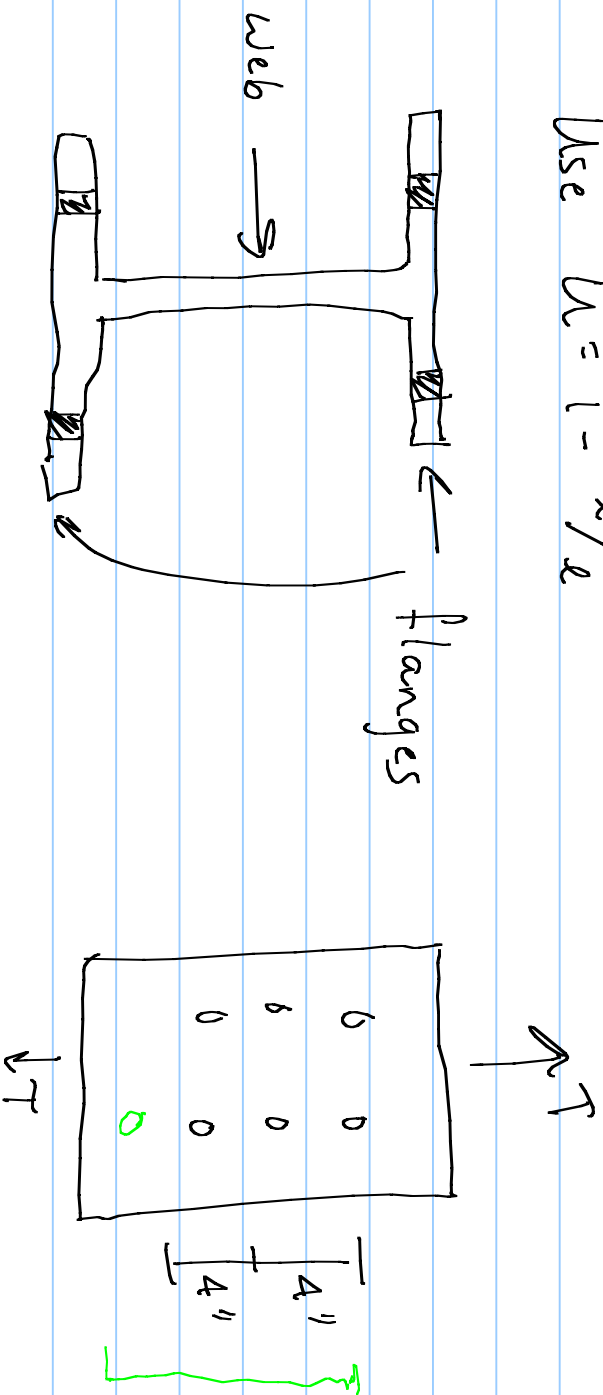
The member is 30' long.

The member has 2 lines of holes in each flange for 1" bolts.

There will be at least 3 bolts in each line, 4" on center.

Use Grade 50 steel.

Use $\phi = 1 - \frac{x}{e}$



$$P_u = 1.2D + 1.6L = 1.2(220) + 1.6(250) = \underline{\underline{664 \text{ kips}}}$$
$$P_u = 1.4D = 1.4(220) = 308 \text{ kips}$$

Area Requirement for Yielding:

$$A_g \geq \frac{P_u}{0.9F_y} = \frac{664}{0.9(50)} = 14.76 \text{ in}^2$$

Area Requirement for Fracture:

$$A_g \geq \frac{P_u}{0.75uF_u} \quad \text{+ } A_{bh}$$

→ Estimate $u \approx 0.8 - 0.9 \Rightarrow$ Assume $u = 0.85$

$$\Rightarrow \text{Estimate } A_{bh} = 4 \left(1 + \frac{1}{8} \right) (0.65) = 2.9 \text{ in}^2$$

estimate

$$A_g \geq \frac{664}{0.75(0.85)(65)} + 2.9 = 18.9 \text{ in}^2$$

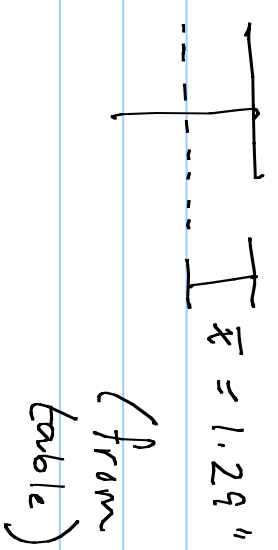
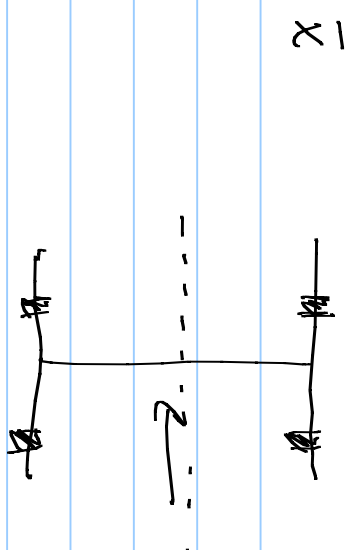
F_u

$$\Rightarrow \text{Try } W14 \times 68 \quad (A_g = 20.00 \text{ in}^2)$$

$$A_{bh} = 4 \left(1 + \frac{1}{8} \right) (0.72) = 3.24 \text{ in}^2$$

$$u = 1 - \frac{x}{L}$$

$$L = 8''$$



W14 x 68

WT 7 x 34

$$U = 1 - \frac{1.29}{8} = 0.84$$

Ag required for fracture: $A_g \geq \frac{664}{0.75(0.84)(65)} + 3.24$

$$A_g \geq 19.5 \text{ in}^2$$

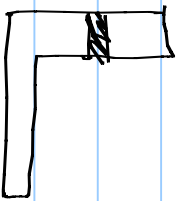
$$A_g = 20.8 > 19.5 \checkmark$$

Slenderness Check : $L/r \leq 300$

$$\frac{(30 \text{ ft}) (12 \text{ in/ft})}{(2.46 \text{ in})} = 146 < 300 \checkmark$$

→ Select W14x68 as lightest acceptable design.

Example 2. Select the lightest Grade 50 angle that can support tension loads 60 kips dead load and 6 kips live load. The member is 12' long. Assume $\frac{7}{8}$ " diameter bolts on a single gage line.



$$P_u = \max \begin{cases} 1.2D + 1.6L = 1.2(60) + 1.6(6) = 82 \text{ kips} \\ 1.4D = 1.4(60) = \underline{\underline{84 \text{ kips}}} \text{ (controls)} \end{cases}$$

$$\text{Required Area for yielding: } A_g \geq \frac{84}{(0.9)(50)} = 1.87 \text{ in}^2$$

Required Area for Fracture :

$$A_g \geq \frac{P_u}{0.75 \phi F_u} + A_{bh}$$

↳ u (from Table D3.1) = 0.8

$$A_{bh} = (1) \left(\frac{7}{8} + \frac{1}{8} \right) t$$

$$A_g \geq \frac{84}{(0.75)(0.8)(65)} + (1)(1)t$$

f	Ag - fracture
$3/16$	2.34
$1/4$	2.40
$5/16$	2.47
$3/8$	2.53
$7/16$	2.59
$1/2$	2.65
$5/8$	2.78
$3/4$	2.90
$7/8$	3.02
1	3.15
$1 1/8$	3.28

Possible Sections	Ag
$4 \times 3 1/2 \times 3/8$	2.67
$5 \times 3 \times 7/16$	3.31
$\checkmark 3 1/2 \times 3 1/2 \times 7/16$	2.65
$3 1/2 \times 3 \times 1/2$	3.00
$3 1/2 \times 2 1/2 \times 3/8$	2.56
$3 1/2 \times 3 1/2 \times 3/8$	2.48
$3 \times 3 \times 7/16$	2.43
$4 \times 4 \times 5/12$	2.40
$\textcircled{*} L5 \times 3 1/2 \times 5/16$	2.56

$Ag = 2.56 > 2.47 \checkmark$

Check Slenderness : $\frac{(12')(12)}{1.02} = 141 < 300 \checkmark$

Use $L5 \times 3\frac{1}{2} \times 5\frac{1}{4}$